

## 表面功能化

# 脲醛树脂包覆对片状羰基铁粉电磁吸波性能的影响

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**摘要:** 目的 提高片状羰基铁粉(FCI)的吸波性能。方法 采用原位聚合法制备脲醛树脂(UF)包覆片状羰基铁粉核壳复合粒子。通过透射电子显微镜(TEM)和X射线衍射仪(XRD)分别对试验前后样品的微观形貌和物相组分进行表征。采用矢量网络分析仪对处理前后片状羰基铁粉在0.5~18 GHz频率范围内的电磁参数进行测试, 基于传输线理论对其反射损耗曲线进行拟合分析。**结果** 微观形貌及X射线衍射谱结果表明, 成功合成了脲醛树脂包覆片状羰基铁粉复合粒子(FCI@UF)。对测得的电磁参数进行分析, 与原始片状羰基铁粉相比, 包覆后铁粉介电常数和磁导率的实部、虚部均呈下降趋势, 电磁波衰减能力减弱, 与空气的阻抗匹配能力增强。反射损耗曲线图中, 包覆后铁粉能有效吸收频带变宽(以反射损耗小于-10 dB的带宽作为有效吸收频带), 由3.15 GHz变为4.38 GHz, 在13.84 GHz时有最小反射损耗(-20.64 dB), 最小反射损耗向高频移动, 最小值降低率达41.38%。**结论** 使用脲醛树脂对片状羰基铁粉进行包覆, 制备了综合吸波性能更具优势的FCI@UF复合粒子, 有效提高了片状羰基铁粉的吸波性能。

**关键词:** 微波吸收; 片状羰基铁粉; 脲醛树脂; 阻抗匹配; 电磁衰减; 反射损耗

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## Effect of Urea Formaldehyde Resin Coating on Electromagnetic Wave Absorption Properties of Flake Carbonyl Iron Powder

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**ABSTRACT:** Flaky carbonyl iron powder (FCI) is a common electromagnetic wave absorbing material, but its resistivity is small, its impedance matching with free space is poor, and wave absorbing performance is not ideal. In order to improve the wave absorbing performance of the flaky carbonyl iron powders, in this paper, urea formaldehyde resin (UF) synthesized by reaction of urea and formaldehyde was used as the wall material, and the flaky carbonyl iron powder was used as the core material. Urea formaldehyde resin coated core shell composite particles (FCI@UF) were prepared by in-situ polymerization. A

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transmission electron microscope (TEM) and an X-ray diffractometer (XRD) were used to characterize the micro morphology and phase composition of the samples before and after the experiment. A Vector network analyzer was used to test the electromagnetic parameters of the flaky carbonyl iron powder before and after treatment in the frequency range of 0.5-18 GHz. Finally, the reflection loss (RL) curve was fitted and analyzed based on the transmission line theory. TEM photos showed that there was a layer of nano film at the edge of FCI obtained after UF treatment. The EDS electronic image and the related element distribution map showed that C, N, O and Fe elements were evenly distributed on the surface of composite particles. Combined with the microscopic morphology and EDS energy spectrum results, it was concluded that this experiment successfully synthesized FCI@UF core shell composite particles. In addition, the characteristic diffraction peaks of FCI and UF appeared in the X-ray diffraction spectra of the treated composite particles, further evidenced successful preparation of FCI@UF composite particles; The electromagnetic parameters measured by the vector network analyzer in the frequency range of 0.5-18 GHz were analyzed. Compared with original FCI, the real and imaginary parts of the coated iron powder dielectric constant and the real and imaginary parts of the magnetic permeability showed a downward trend. The tangent value of the loss angle could represent the electromagnetic wave loss capacity of the absorbing material. The tangent value of FCI@UF composite material loss angle also decreased, indicating that the attenuation ability of electromagnetic wave was weakened. But through analysis, the impedance matching ability of FCI@UF composite material with air was enhanced, so it was impossible to directly determine the strength of electromagnetic wave absorbed by the material. The reflection loss simulation calculation was conducted according to the measured electromagnetic parameters. The wave absorption performance of the absorbing material could be directly observed by using the reflection loss curve. In the reflection loss curve, the effective absorption band of coated iron powder became wider (the band with the reflection loss less than -10 dB was taken as the effective absorption band), changing from 3.15 GHz to 4.38 GHz, at 13.84 GHz, the minimum reflection loss was -20.64 dB, and the minimum reflection loss moved to high frequency, with a minimum reduction rate of 41.38%. In a word, this paper uses urea formaldehyde resin to coat the flaky carbonyl iron powders, and prepares the FCI@UF composite material, effectively improving the microwave absorbing performance of the FCI composite material.

**KEY WORDS:** microwave absorption; flake carbonyl iron powder; urea formaldehyde resin; Impedance matching; electromagnetic attenuation; reflection loss

随着现代光电磁探测技术的发展,出现了各类可见光、雷达、红外等探测器,为提高隐蔽性能,尽可能降低被发现、识别、跟踪的概率,隐身技术应运而生<sup>[1-5]</sup>。所谓隐身技术,就是通过优化目标外形设计、在目标表面使用隐身材料进行涂装等手段,尽可能降低目标的可探测信号特征<sup>[6]</sup>。据统计,目前使用的所有目标探测手段中雷达探测约占 60%,且雷达探测技术最为成熟,因而成为近年来的研究热点之一<sup>[7]</sup>。

实现雷达隐身常用的 2 种技术手段是外形设计和制备雷达吸波材料<sup>[8]</sup>。改变外形设计来实现隐身在实际应用中存在较多缺陷,特定结构的外形设计会使装备的生产难度加大,生产成本提高,受到结构力学、空气动力学等多种条件限制,预计不久的将来,通过外形设计实现的隐身效果将达到上限<sup>[9-10]</sup>,和制备吸波材料相比实际应用价值小,以致吸波材料研究成为发展和应用雷达隐身技术的主要手段<sup>[11]</sup>。球形碳基铁粉是应用较早的一类吸波材料,因为具有高的饱和磁化强度、高的磁导率和居里温度,制备的涂层在较薄厚度下对雷达波有强烈的吸收效能,在雷达吸波材料领域表现出广泛的应用前景。球形碳基铁粉通过简单物理球磨后得到的片状碳基铁粉具有更好的吸波效率,FCI 厚度薄于碳基铁材料趋肤深度,可减小趋肤

效应对铁粉的影响;另外,薄片形状具有平面各向异性,能够突破 Snoek 极限限制,从而在高频波段仍能保持较高的磁导率<sup>[12-14]</sup>。尽管 FCI 具有较好的电磁波衰减特性,但是在制备涂层时,由于 FCI 的片状特性,片状粒子在基体中与其他片状粒子通过面接触相互搭接形成的覆盖或重叠结构,相比于 CIP 在基体中粒子间的点接触,更有利于建立连续和广泛的导电网络,增加涂层的电导率和介电常数实部<sup>[15]</sup>,导致空气与涂层之间阻抗匹配特性较差,阻碍更多电磁波入射进吸波涂层内部,无法获得理想的电磁波吸收性能<sup>[16-19]</sup>。因此,为了提高 FCI 的阻抗匹配特性,研究者们通常采用有机或无机包覆来调节其电磁参数,提高其整体电磁波吸收特性。例如,黄赤等<sup>[20]</sup>采用正硅酸乙酯、磷酸等分别对片状碳基铁粉进行包覆处理,结果表明,包覆绝缘层后的样品在不影响磁导率的同时,显著提高了片状碳基铁粉的电阻率和阻抗匹配特性,并降低了介电常数。Han 等<sup>[21]</sup>采用化学沉淀法在片状碳基铁粉表面包覆了 ZnO 纳米壳,与未处理的片状碳基铁粉相比,FCI@ZnO 复合粒子的介电常数较低,且反射损耗 (RL) 显著提高,最小 RL 在 1.96 GHz 时达到-31.93 dB,匹配厚度为 2.5 mm,有效提高了材料整体的吸波性能。上述文献表明,绝缘包覆作为

一种有效手段, 能够提高片状羰基铁粉的阻抗匹配特性, 从而改善其吸波性能。但上述研究大多集中在无机包覆, 对有机包覆研究甚少<sup>[22-26]</sup>。脲醛树脂是一种常用的有机微胶囊壁材材料, 具有制备工艺简单、耐酸碱、耐磨、绝缘性能优异等优点<sup>[27]</sup>, 上述性能对复合片状羰基铁粉的电磁波吸收性能有待进一步研究。

本试验中选择片状羰基铁粉作为主吸收剂, 采用原位聚合法在铁粉表面包覆一层脲醛树脂薄膜, 拟制备核壳状脲醛树脂包覆片状羰基铁粉复合粒子, 利用脲醛树脂较低的电导率来提高最终产物与空气的阻抗匹配特性, 实现片状羰基铁粉吸波性能的优化, 从而扩大其应用场景和使用范围。

## 1 试验

### 1.1 原料

原材料包括: 片状羰基铁粉(微米级), 分析纯, 长沙利友金属材料有限公司, 片状羰基铁粉需要经丙酮超声清洗后, 在真空烘箱中烘干方可备用; 尿素、甲醛(质量分数37%)、盐酸(质量分数37%)、氯化铵、正辛醇、丙酮、无水乙醇, 分析纯, 国药集团化学试剂有限公司(质量分数为37%的盐酸需要用蒸馏水稀释至质量分数为1%的稀盐酸, 备用); 间苯二酚, 分析纯, 上海麦克林工业生产园; OP-10, 天津市致远化学试剂有限公司; 蒸馏水, 分析纯, 大友化工原料有限公司。

### 1.2 制备过程

以尿素、甲醛反应合成的脲醛树脂(UF)为壁材, 片状羰基铁粉(FCI)为芯材, 通过原位聚合法制备片状羰基铁粉@脲醛树脂核壳复合粒子(FCI@UF)。具体步骤为: 室温下量取100 mL蒸馏水加入烧杯中, 滴加1 g OP-10, 搅拌至完全溶解后获得1%的OP-10乳化剂水溶液, 称取一定质量的尿素、氯化铵、间苯二酚加入烧杯中, 缓慢滴加1%稀盐酸调节溶液pH至3左右, 在1200 r/min下乳化15 min, 将乳液移至四口烧瓶中, 用氮气瓶向四口烧瓶中通氮气, 排除四口烧瓶中的空气, 在制备过程中一直通氮气保护, 将烘干处理后的3 g 羰基铁粉加入混合液, 搅拌均匀, 称取2倍尿素质量的甲醛溶液, 缓慢加入到四口烧瓶中, 在60 ℃水浴加热条件下, 以1500 r/min速率持续搅拌反应5 h, 真空抽滤得到反应产物, 用蒸馏水和丙酮洗涤2~3次, 将得到的滤饼在50 ℃下干燥至恒重。

### 1.3 性能测试及表征手段

为了表征包覆是否成功, 采用美国FEI Tecnai G2F 20型透射电子显微镜, 观察脲醛树脂包覆前后片状羰基铁粉的微观结构和形貌。借助Malvern Panalytical EMPYREAN SERIES 3型X射线衍射仪

(XRD, Cu靶K $\alpha$ 线辐射), 对包覆前后羰基铁粉的物相进行分析, 测试参数为: 扫描电压40 kV, 电流40 mA。为获得样品的电磁参数, 采用Keysight P5004A型矢量网络分析仪通过同轴法进行测试, 将样品按40%的质量比与固体石蜡在加热台上均匀混合, 用压片机压成外径7 mm、内径3.04 mm、厚度约3 mm的同轴环, 在0.5~18 GHz频率范围内测试。为评价吸波材料的吸波性能, 利用传输线理论对矢量网络分析仪测得的电磁参数进行模拟计算分析, 获得材料的电磁波反射损耗曲线。

## 2 结果与讨论

### 2.1 形貌及成分分析

脲醛树脂处理前后片状羰基铁粉的TEM和HRTEM图像如图1所示。对比图1a和图1d发现, 原始片状羰基铁粉成薄片状, 脲醛树脂包覆后片状羰基铁粉与原始片状羰基铁粉形态相似。通过观察分析发现, 脲醛树脂处理后获得的FCI@UF复合粒子边缘处有一层纳米薄膜(图1a~b), 厚度约为35.7 nm, 证明了脲醛树脂包覆羰基铁被成功制备。图1c为FCI的高分辨率透射电镜图像, 其晶面间距为0.204 nm, 对应 $\alpha$ -Fe的(110)晶面<sup>[28]</sup>。图1f未观察到清晰可见的晶格条纹, 进一步表明片状羰基铁粉被成功包覆。图2为EDS电子图像和相关元素分布图, FCI@UF复合粒子表面均匀地分布着C(图2b)、N(图2c)、O(图2d)、Fe(图2e)元素, 且从图2f观察到FCI@UF复合粒子表面, Fe元素密度由中心向外逐渐降低, 尤其在边缘处Fe元素的分布明显减少, C、N、O元素较多, 表明图1e中出现的薄膜为脲醛树脂<sup>[29]</sup>。结合TEM图和能谱分析结果, 能够确定片状羰基铁粉表面上成功包覆脲醛树脂薄膜, 该薄膜的制备不仅能够改善纯羰基铁吸波剂的阻抗匹配, 提高综合吸波性能, 还能有效隔离羰基铁与空气的接触, 增加其抗氧化性能。

### 2.2 物相分析

为进一步确定样品物相组成, 采用XRD对其进行表征。图3中为UF、FCI和FCI@UF复合粒子的XRD图。对于脲醛树脂, 在 $2\theta$ 为21.65°、24.13°处均有明显的衍射峰, 与文献<sup>[30-31]</sup>中提到的衍射峰一致。在片状羰基铁粉的XRD图中, 在44.77°附近有明显的衍射峰, 在65.02°处有较弱的衍射峰, 其分别对应立方 $\alpha$ -Fe(JCPDS No.87-0721)的(110)和(200)晶面<sup>[32]</sup>。在FCI@UF复合粒子的XRD图中, 除了立方 $\alpha$ -Fe的衍射峰, 在 $2\theta$ 为21.65°、24.13°处均存在明显的衍射峰, 对应UF, 进一步证明成功制备了FCI@UF复合粒子。图中FCI@UF复合粒子在44.77°附近的衍射峰明显减弱, 这与脲醛树脂的包覆有关。

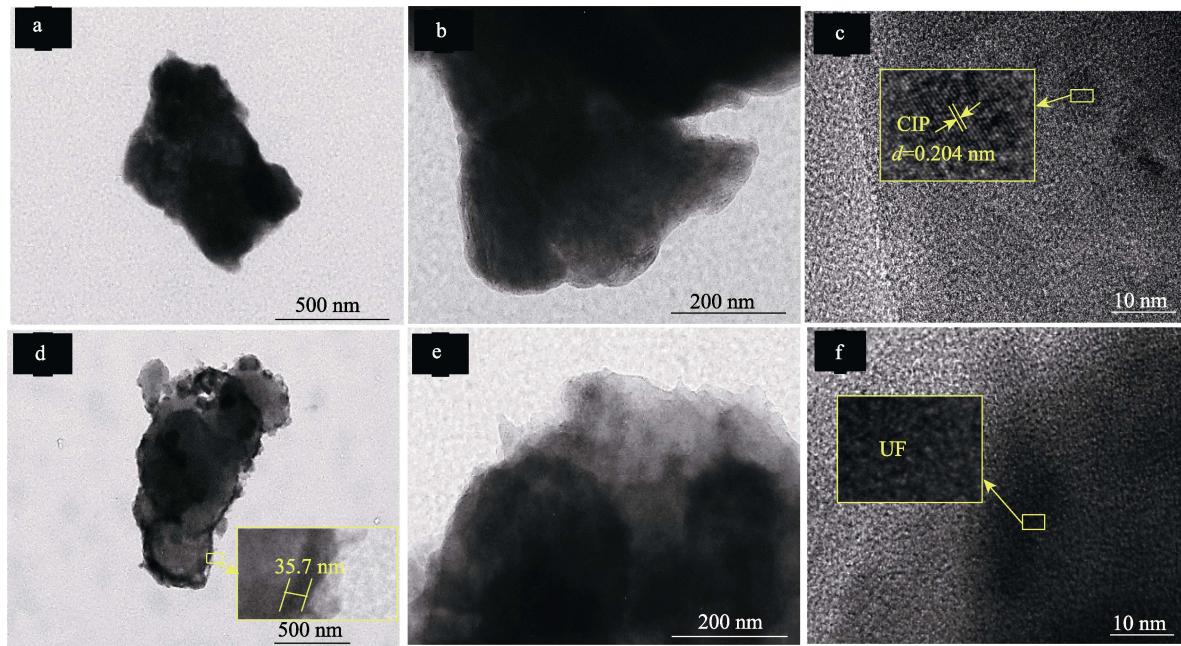


图1 FCI粒子的TEM照片(a~b)和HRTEM照片(c)以及FCI@UF复合粒子的TEM照片(d~e)和HRTEM照片(f)

Fig.1 TEM (a-b) and HRTEM (c) of FCI and TEM (d-e) and HRTEM (f) of FCI@UF composite particles

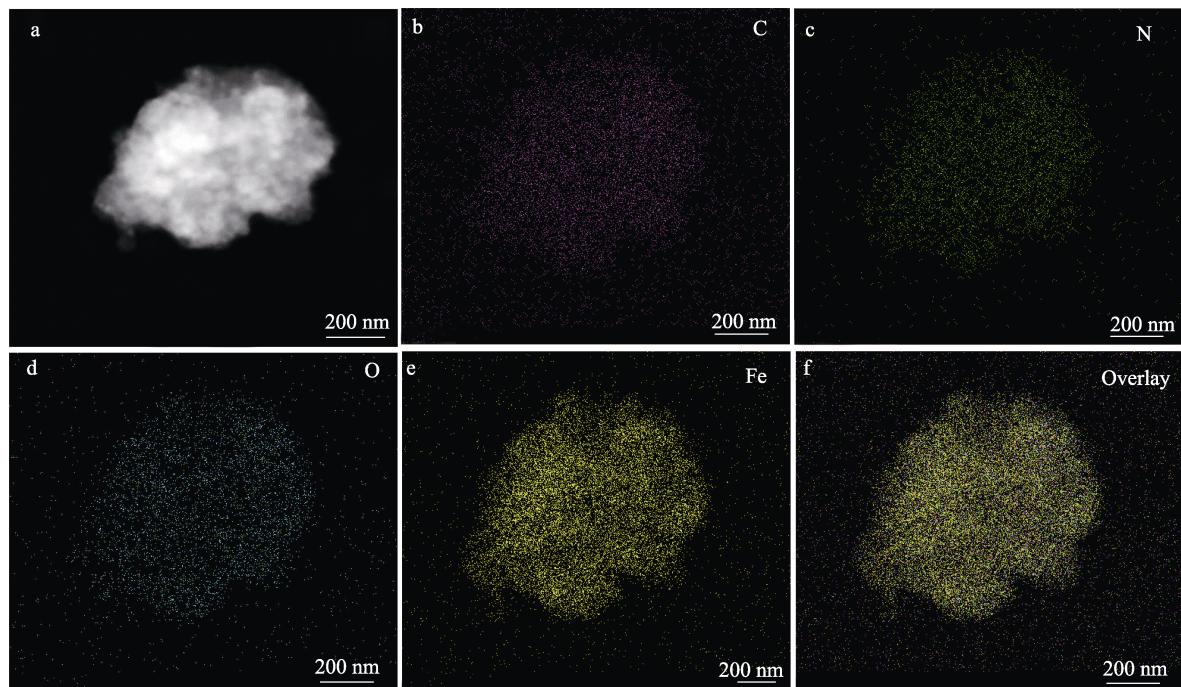


图2 片状羰基铁粉/脲醛树脂复合粒子的TEM图像(a)和EDS元素分布图(b~f)

Fig.2 TEM image (a) and EDS element distribution diagram (b-f) of sheet carbonyl iron powder/urea formaldehyde resin composite particles

### 2.3 包覆前后铁粉电磁参数分析

图4为未处理片状羰基铁粉和脲醛树脂包覆后片状羰基铁粉介电常数随频率的变化曲线。从图中可以看出,包覆脲醛树脂的片状羰基铁粉介电常数的实部和虚部都有下降,实部下降趋势更为明显。在微波波段,羰基铁粉介电常数实部 $\epsilon'$ 主要取决于界面极

化和电子位移极化<sup>[33]</sup>,一方面,当脲醛树脂包覆片状羰基铁粉后,FCI@UF复合粒子尺寸变大,分别使用相同含量的原始FCI和FCI@UF制备复合材料,FCI@UF与基体材料间的异质结构界面减少,电介质中电子或离子在界面处俘获量减少,在外电磁场作用下FCI@UF复合材料相比于FCI复合材料界面极化降低,所以FCI@UF复合粒子介电常数实部明显小

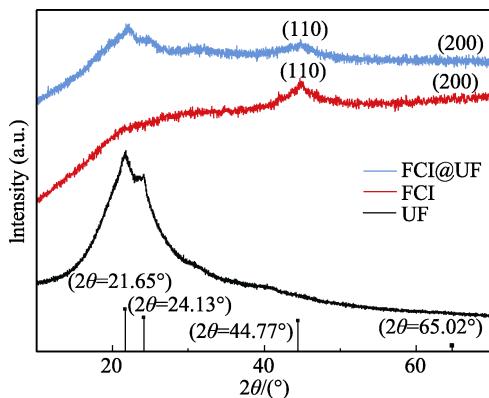


图 3 FCI@UF、FCI、UF 的 XRD 图谱  
Fig.3 X-ray diffraction pattern of FCI@UF, FCI, UF

于原始 FCI 粒子<sup>[18-19,34]</sup>; 另一方面, 羰基铁粉在交变电场中容易产生电子位移极化, 特别是片状羰基铁粉, 片与片之间相互搭接形成导电网络, 更有利于电子通过迁移、跳跃和隧穿等方式在 FCI 导电网络中传输, 产生强烈的电导损耗, 实现电磁衰减, 而电绝缘性脲醛树脂的包覆在片状羰基铁粉表面形成了一层纳米厚度的绝缘薄膜, 造成 FCI@UF 复合粒子单元之间难以形成导电网络, 基体材料中构建的局部导电网络不完善, 阻碍了自由电子在导电网络中快速定向迁移<sup>[16,18-19,21]</sup>, 导致 FCI@UF 复合材料介电常数实部减小。此外, 通过自由电子理论<sup>[35]</sup>:  $\epsilon'' \approx \sigma / (2\pi\epsilon_0 f)$

( $\sigma$  为电导率), 其中,  $\epsilon_0$  和  $f$  分别为真空中的介电常数值和频率。因此, 介电常数的虚部  $\epsilon''$  与电导率  $\sigma$  成正比关系, FCI@UF 复合材料的介电常数虚部随电导率减小而下降。另外, 由图 4 可知, FCI@UF 复合材料的介电常数实部和虚部随频率的升高, 其变化趋势更加平稳, 表现出比 FCI 更好的频散特性<sup>[36]</sup>, 这表明脲醛树脂包覆手段能够有效提高片状羰基铁粉吸波性能的稳定性。

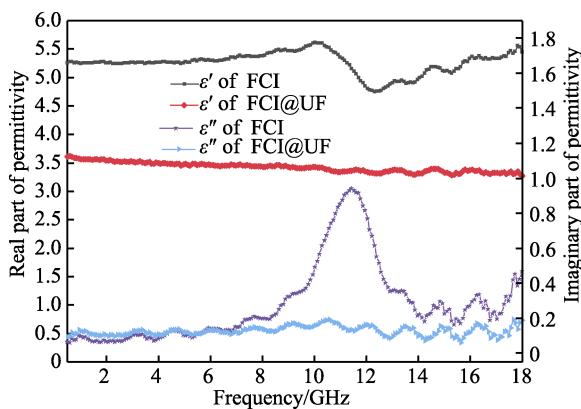


图 4 FCI、FCI@UF 复合材料介电常数随频率的变化曲线  
Fig.4 Change of dielectric constant of FCI, FCI@UF composites with frequency

图 5 为 FCI@UF 复合材料复磁导率随频率的变化, 可知脲醛树脂包覆后, 片状羰基铁粉磁导率的实部和虚部也都表现出减小趋势, 但两者变化幅度相对

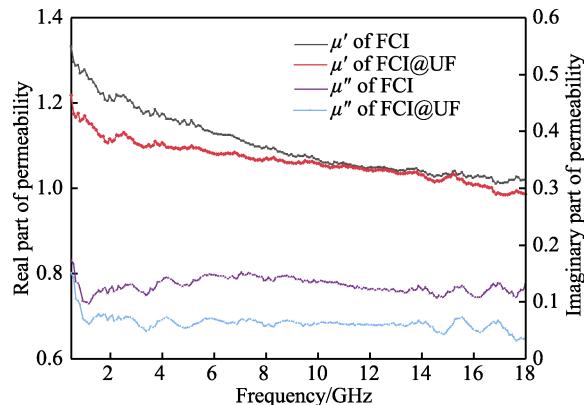


图 5 FCI、FCI@UF 复合材料磁导率随频率的变化曲线  
Fig.5 Change of permeability of FCI, FCI@UF composites with frequency

于介电常数较小。对于磁导率变化, 其原因主要有: 当非磁性 UF 包覆 FCI 后, 脲醛树脂薄层的存在将降低磁性吸收剂中铁粉的质量分数, 同时在试验过程中 FCI 不可避免地被氧化, 导致磁导率下降<sup>[23]</sup>; 非晶态电介质相 UF 处于磁性 FCI 之间, 削弱 FCI 之间的磁相互作用, 减弱了铁粉颗粒之间由于磁耦合造成的磁损耗<sup>[19,37]</sup>, 另外非磁性 UF 层厚度较小, 不会在填料-基体界面上造成无序, 仅仅在一定程度上削弱磁性颗粒之间的磁相互作用<sup>[38]</sup>, 因此 FCI@UF 复合材料的磁导率实部  $\mu'$  和虚部  $\mu''$  会下降。

## 2.4 衰减特性和阻抗匹配性能分析

吸波涂层材料完成吸波需要 2 个过程: 首先, 当电磁波从空气入射到吸波涂层材料表面时, 电磁波能够尽可能多地入射到材料内部而不被表面反射; 其次, 进入到材料内部的电磁波需要被快速地吸收耗散掉, 达到隐身的目的。即作为吸波材料必须具备 2 个条件: 阻抗匹配和衰减特性<sup>[19]</sup>。

材料损耗电磁波能力的强弱体现了材料的衰减特性, 用损耗角正切值表示吸波材料的电磁波损耗能力<sup>[39]</sup>:

$$\tan \delta = \tan \delta_m + \tan \delta_e \quad (1)$$

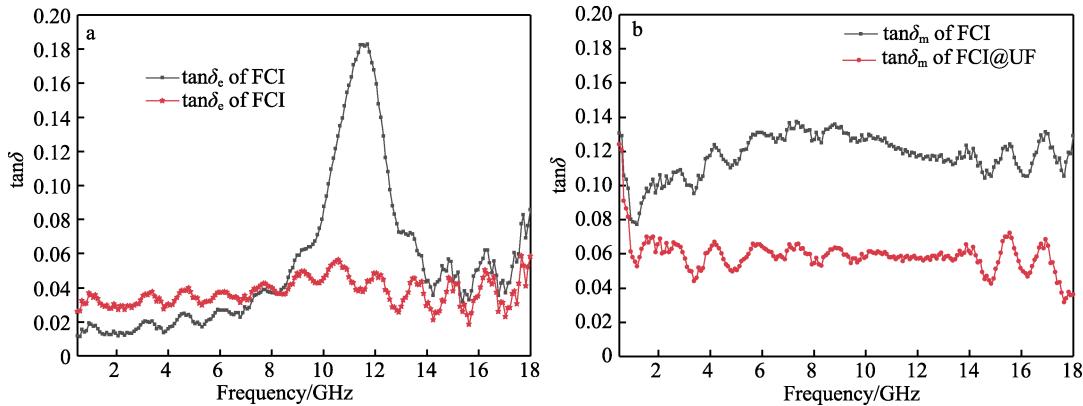
$$\tan \delta_m = \mu'' / \mu' \quad (2)$$

$$\tan \delta_e = \epsilon'' / \epsilon' \quad (3)$$

式中:  $\tan \delta$  为材料的损耗角正切值。损耗角正切值  $\tan \delta$  由介电损耗角正切  $\tan \delta_e$  和磁损耗角正切  $\tan \delta_m$  组成, 即  $\tan \delta_e$  和  $\tan \delta_m$  决定了材料对电磁波的损耗能力。从图 6 中可以看出, FCI@UF 复合材料的  $\tan \delta_e$  和  $\tan \delta_m$  均呈减小的趋势, 说明脲醛树脂包覆之后片状羰基铁粉的电磁波损耗能力减弱。

当电磁波从空气环境入射到具有介电损耗和磁损耗能力的吸波材料表面时, 吸波材料的反射系数  $R$  能够体现吸波材料与空气的阻抗匹配特性<sup>[40]</sup>:

$$R = \frac{\sqrt{\frac{\mu_r}{\epsilon_r}} - 1}{\sqrt{\frac{\mu_r}{\epsilon_r}} + 1} \quad (4)$$

图 6 FCI 和 FCI@UF 复合材料的  $\tan \delta_e$  (a) 和  $\tan \delta_m$  (b) 随频率的变化Fig.6 Change of  $\tan \delta_e$  (a) and  $\tan \delta_m$  (b) of FCI and FCI@UF composites with frequency

式中:  $\mu_r$  和  $\varepsilon_r$  分别为材料的相对复磁导率和相对复介电常数,  $\mu_r = \mu' - i\mu''$ ,  $\varepsilon_r = \varepsilon' - i\varepsilon''$ 。由公式(4)可知, 材料相对复磁导率和相对复介电常数比值越接近于1, 材料反射系数  $R$  越小, 吸波性能越好。查阅相关文献<sup>[41]</sup>发现, FCI 的相对复介电常数大于相对复磁导率。观察图 4 发现, 脲醛树脂包覆后, 片状碳基铁粉的介电常数实部  $\varepsilon'$  下降较快, 由  $\varepsilon_r = \varepsilon' - i\varepsilon''$  可知, 材料相对复介电常数  $\varepsilon_r$  减小。由图 5 可知, 包覆后铁粉磁导率虚部  $\mu''$  下降得比磁导率  $\mu'$  实部快, 特别是在 8~18 GHz 频率范围内, FCI@UF 复合材料的磁导率实部  $\mu'$  基本不变, 这说明包覆后铁粉相对复磁导率  $\mu_r$  显著增大。由公式(4)可知,  $\varepsilon_r$  减小,  $\mu_r$  增大,  $\mu_r/\varepsilon_r$  更加接近于1, 反射系数  $R$  减小, 因此与原始 FCI 复合材料相比, FCI@UF 复合材料表面反射的电磁波减小, 与空气阻抗匹配性能增强<sup>[37,42]</sup>。

## 2.5 吸波性能改善机理

相比于未处理 FCI, FCI@UF 复合材料对电磁波衰减能力减弱、与空气阻抗匹配性能增强, 可以通过电磁波反射损耗 (RL) 直接判定材料吸收电磁波的强弱, 观测吸波材料的吸波性能。根据传输线理论, 在吸收层厚度和频率已知的条件下, 通过实际测量的电磁参数可以计算以金属为衬底单层吸波涂层的反射损耗<sup>[43]</sup>:

$$S_{RL} = 20 \lg |(Z_{in} - Z_0) / (Z_{in} + Z_0)| \quad (5)$$

$$Z_{in} = Z_0 (\mu_r / \varepsilon_r)^{1/2} \tan h[j(2\pi f d / c)(\mu_r \varepsilon_r)^{1/2}] \quad (6)$$

式中:  $Z_{in}$  和  $Z_0$  分别为吸波材料的输入阻抗和空气的特征阻抗,  $d$  为吸收层的厚度,  $c$  为光速,  $f$  为电磁波的频率。

模拟吸收层计算厚度为 6 mm 时, FCI 和 FCI@UF 复合材料的反射损耗曲线如图 7 所示。FCI 复合材料在 0.5~18 GHz 频率范围内, 反射损耗小于-10 dB 的有效吸收频带范围为 8.46~11.61 GHz (带宽 3.15 GHz), 在 9.51 GHz 处最小反射损耗值为-12.10 dB。而 FCI@UF 复合材料在 13.84 GHz 时有最小的反射损

耗, 为-20.64 dB, 反射损耗小于-10 dB 的频率范围为 11.00~15.38 GHz (带宽 4.38 GHz)。相比于 FCI 复合材料, FCI@UF 复合材料的反射损耗有效吸收频带和峰值都向高频移动, 有效吸收带宽略有增加, 最小反射损耗小于-20 dB, 其原因是: 碳基铁表面包覆的绝缘性脲醛树脂层屏蔽了材料整体的电荷性, 削弱了碳基铁表面电子由于位移极化而产生的极化强度, 从而降低了复介电常数实部, 并有效改善了吸波涂层的阻抗匹配能力, 促使更多的电磁波进入涂层内部而被损耗掉, 增大了有效吸收带宽, 减小了最小反射损耗。另外, 由吸波涂层最小反射损耗所对应的频率满足关系式<sup>[28]</sup>:

$$f_m = \frac{c}{4d\sqrt{\varepsilon_r \mu_r}} \quad (7)$$

式中:  $f_m$  为匹配频率, 对应着吸波涂层反射损耗曲线峰值 (最小反射损耗) 频率。根据公式(7)可知, 在涂层厚度  $d$  不变的前提下, 匹配频率与相对复磁导率和相对复介电常数的乘积成反比, 包覆脲醛树脂后降低了片状碳基铁粉的  $\varepsilon_r$  和  $\mu_r$ , 匹配频率升高, 因此 FCI@UF 复合材料的反射损耗有效吸收频带和峰值都向高频移动。由上述分析可知, 尽管处理后铁

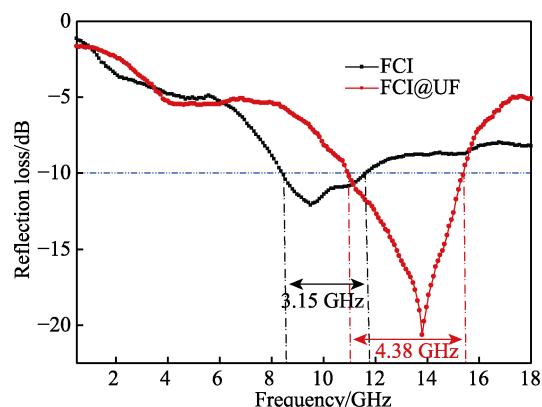


图 7 FCI 和 FCI@UF 复合材料的反射损耗对比 (厚度 6 mm)

Fig.7 Comparison of reflection loss of FCI and FCI@UF composites (thickness 6 mm)

粉的反射损耗曲线中有效吸收频带和峰值往高频方向偏移, 但是粉体的阻抗匹配性能得到了改善, 吸收强度和吸收宽度也相应提高。与 FCI 复合材料相比, FCI@UF 复合材料的综合吸波性能更优。

### 3 结论

1) 利用原位聚合法对片状羰基铁粉进行包覆改性, TEM 图像显示片状羰基铁粉边缘处形成了明显的纳米薄膜, 结合 EDS 与 XRD 结果, 可知片状羰基铁粉@脲醛树脂核壳复合粒子成功制备。

2) 由于脲醛树脂在片状羰基铁粉表面形成了绝缘包覆层, 阻碍了片状羰基铁粉本征的界面极化和电子位移极化, FCI@UF 复合材料与 FCI 复合材料相比, 介电常数和磁导率的实部、虚部均下降, 介电常数实部由 4.7~5.8 降至 3.5 左右, 与介电常数实部的降幅相比, 其他电磁参数的变化较小。

3) 与 FCI 复合材料相比, FCI@UF 复合材料的综合吸波性能更优。进一步对测得的电磁参数进行分析, 与 FCI 相比, FCI@UF 核壳复合粒子对电磁波衰减能力减弱、与空气阻抗匹配能力增强。借助反射损耗模拟结果, 在模拟吸收层计算厚度为 6 mm 时, 包覆后的羰基铁粉吸收层与原铁粉吸收层相比, 有效吸收频带和峰值都向高频移动, 最小反射值由 -12.10 dB 降低至 -20.64 dB, 最小值降低率达 41.38%, 有效吸收带宽由 3.15 GHz 拓宽至 4.38 GHz。

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